

# Dielectric resonators in BaO–Ln<sub>2</sub>O<sub>3</sub>–5TiO<sub>2</sub> system (Ln = La, Pr, Nd, Sm)

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*Ceramics of composition BaO–Ln<sub>2</sub>O<sub>3</sub>–5TiO<sub>2</sub> have been prepared with four lanthanide elements (Ln = La, Pr, Nd, Sm) by a conventional solid state ceramic preparation route and the dielectric properties measured in the microwave frequency range. The dielectrics had high values for the dielectric constant  $\epsilon_r$  in the range 72–88 and quality factor  $Q_u$  values of up to 24 000. The phase constitution and microstructures of the materials were characterised using X-ray diffraction and scanning electron microscopy, respectively. The observed properties indicate that these are promising materials for use as microwave dielectric resonators.*

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## INTRODUCTION

With the increasing demand for miniaturisation of microwave communication systems such as cellular telephones, ceramic dielectrics with high permittivity and low loss have become indispensable for microwave integrated circuits (MICs). These ceramics, called 'dielectric resonators' (DRs) offer small size, light weight, temperature stability, and integrability by virtue of the unique combination of properties they possess.<sup>1,2</sup> Ceramics used for DR applications need relative permittivity or dielectric constant  $\epsilon_r$  in the range 25–100,  $\tan \delta < 5 \times 10^{-4}$ , where  $\tan \delta$  is dielectric loss, and  $\tau_f$  (coefficient of thermal variation of resonant frequency) within  $\pm 20$  ppm  $K^{-1}$ . The resonant frequency of a DR (usually  $TE_{018}$  for practical applications) is selected by taking the  $\epsilon_r$  of the material and the dimensions into consideration. In pursuit of appropriate materials, a few ceramics such as Ba<sub>2</sub>Ti<sub>9</sub>O<sub>20</sub> (Refs. 3–5), (Zr,Sn)TiO<sub>4</sub> (Refs. 6–8), Ba(Zn,Ta)O<sub>3</sub> (Refs. 9–11), Ba(Mg,Ta)O<sub>3</sub> (Ref. 12), Ba(Re,Nb)O<sub>3</sub> (Refs. 13, 14), Ba<sub>5</sub>Nb<sub>4</sub>O<sub>15</sub> (Ref. 15) have been investigated. All the above ceramics have  $\epsilon_r < 45$  and hence their use in 800 MHz band is limited by the large size. Development of microwave dielectric resonators still with high  $\epsilon_r$  is required for frequencies  $< 2$  GHz where the wavelength is large, and can be reduced through high  $\epsilon_r$  dielectrics. A dielectric constant in the range 70–90 is commonly needed in the 800 MHz mobile telephone system and in L or S band frequencies for miniaturisation of circuits. More recently BaNd<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub> and BaSm<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub> have been reported<sup>16–26</sup> as high  $\epsilon_r$  dielectric ceramics for the above applications. The  $\epsilon_r$  of BaNd<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub> based materials varies in the range 77–95 and  $\tau_f$  from +90 to +123 whereas in BaSm<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub> based ceramics  $\epsilon_r$  varies in the range 66–77 and  $\tau_f$  from –30 to +12. The quality factor varies from 1000 to 20 000. These variations in the dielectric properties are attributed<sup>16–26</sup> to the presence of secondary phases such as Ba<sub>2</sub>Ti<sub>9</sub>O<sub>20</sub>, BaTi<sub>4</sub>O<sub>9</sub>, TiO<sub>2</sub>, Nd<sub>2</sub>Ti<sub>2</sub>O<sub>7</sub>, Sm<sub>2</sub>Ti<sub>2</sub>O<sub>7</sub>, etc. Partial substitution of Ba by Sr or Pb or

addition of Bi<sub>2</sub>O<sub>3</sub> enhances the  $\epsilon_r$  and improves  $\tau_f$  in the above systems.<sup>16,17,19,24</sup> In the present paper the preparation, characterisation, and dielectric properties of BaLn<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub> (Ln = La, Pr, Nd, Sm) are reported.

## EXPERIMENTAL PROCEDURES

### Sample preparation

High purity BaCO<sub>3</sub>, TiO<sub>2</sub>, La<sub>2</sub>O<sub>3</sub>, Pr<sub>2</sub>O<sub>3</sub>, Nd<sub>2</sub>O<sub>3</sub> and Sm<sub>2</sub>O<sub>3</sub> were mixed in the molecular proportions BaO:Ln<sub>2</sub>O<sub>3</sub>:TiO<sub>2</sub> = 1:1:5 with distilled water for ~30 min in an agate mortar. The powders were calcined in alumina crucibles at 1120–1200°C for 4 h with intermediate grinding, then mixed with PVA binder, and ground for 1 h. They were pressed into 10 mm diameter compacts at 350 MPa and subsequently sintered in air at 1300–1350°C for 4 h. The density of the sintered compacts was determined from the dimensions. X-ray diffraction (XRD) studies were carried out on powdered samples using Cu K $\alpha$  radiation and the microstructures examined by SEM.

### Microwave dielectric property measurements

The dielectric constant was measured using an HP 8510 B network analyser and accessories by the post resonator method as proposed by Hakki and Coleman<sup>27</sup> and modified by Courtney.<sup>28</sup> First, the cylindrical sample is resonated in the end shorted condition. The E-field probes couple the microwave to the sample and the  $TE_{018}$  resonance corresponding to a frequency  $f_0$  in the transmission mode is taken. Using a Hewlett Packard 9000/300 series computer, which controls the network analyser, the  $\epsilon_r$  is calculated using the relation

$$\epsilon_r = 1 + \left( \frac{\lambda_0}{\pi D} \right)^2 (\alpha_1^2 + \beta_1^2) \quad (1)$$

where  $\beta_1$  is a function of the resonant frequency and sample dimensions given by

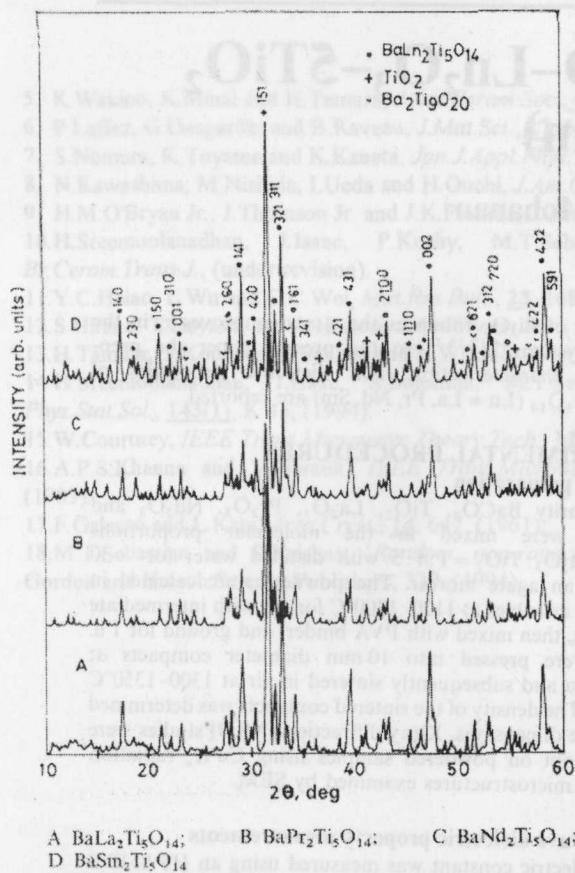
$$\beta_1 = \frac{\pi D}{\lambda_0} \left[ \left( \frac{\lambda_0}{2L} \right)^2 - 1 \right]^{1/2} \quad (2)$$

Here,  $\lambda_0$  is the free space wavelength corresponding to  $f_0$ , and  $D$  and  $L$  are the specimen diameter and height respectively.  $\alpha_1$  is taken from a mode chart given in Ref. 27. The selection of resonant frequency and the calculation of  $\epsilon_r$  are done entirely by the computer.

The conduction loss in the above method is quite high and comparable to the loss of the dielectric material itself.<sup>1</sup> Hence this method cannot be used for the  $Q_u$  measurement. In this work the 'stripline method' proposed by Khanna and Garault<sup>29</sup> for estimating the  $Q_u$  value was used. In this method the dielectric ceramic coupled to a stripline of 50  $\Omega$  acts as a band rejection filter. The least transmission coefficient  $S_{21u}$  corresponding to  $f_0$  is taken. From this, the width of the resonant curve  $\Delta f$  corresponding to the transmission coefficient  $S_{21u}$  given by

$$S_{21u} = S_{21} \left( \frac{2}{1 + S_{21}^2} \right)^{1/2} \quad (3)$$

is taken. The unloaded quality factor,  $Q_u$ , is calculated from



1 Powder X-ray diffraction patterns of BaLn<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub> ceramics obtained using Cu K<sub>α</sub> radiation

the relation

$$Q_u = f_0 / \Delta f \quad (4)$$

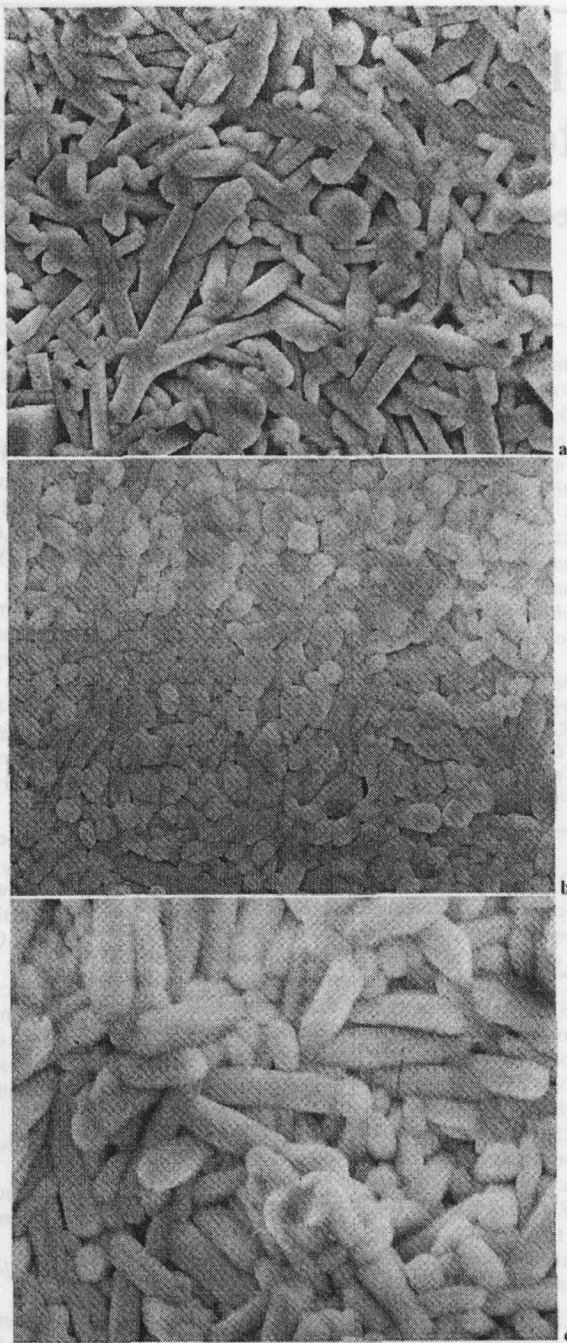
Here, also, the frequency selection and the calculation are completely done by the computer. This method is straightforward and is reproducible. Moreover, the  $Q$  value obtained is almost equal to  $Q_u$  since proper shielding is provided (using a brass cavity of size  $5 \times 5 \times 3$  cm) to prevent radiation loss. Most of the applications of DR involve coupling using striplines. In fact, the present method is superior to all other existing methods since the measurement is made in an actual working environment.

The temperature variation of the resonant frequency  $\tau_f$  was obtained by placing the ceramic at the centre of the bottom of an aluminium cavity, 4 cm dia.  $\times$  7 cm high, and by keeping the top open. Here the cavity dimensions are four times those of the dielectric ceramic. Using an E-field probe, the resonant frequency  $f_0$  and the shift during heating were determined in the range 25–80°C. A graph drawn between resonant frequency and temperature, whose slope gives  $\Delta f / \Delta T$  and the  $\tau_f$ , was obtained using the following equation

$$\tau_f = \frac{1}{f_0} \left( \frac{\Delta f}{\Delta T} \right) \quad (5)$$

## RESULTS AND DISCUSSION

The powder XRD patterns obtained for the four ceramics, BaLa<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub>, BaPr<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub>, BaNd<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub>, and BaSm<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub> are shown in Fig. 1. The patterns are similar for all the samples and show that the 1:1:5 is the major



a BaPr<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub>,  $\times 3000$ ; b BaNd<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub>,  $\times 3000$ ; c BaSm<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub>,  $\times 4000$

## 2 SEM of BaLn<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub> ceramics

phase. The patterns contain additional diffraction peaks corresponding to that of Ba<sub>2</sub>Ti<sub>9</sub>O<sub>20</sub> and TiO<sub>2</sub>. The microwave dielectric properties such as  $\epsilon_r$ ,  $Q_u \times f$ , and  $\tau_f$  are shown in Table 1. A study of Table 1 indicates that, in general,  $\epsilon_r$  and  $\tau_f$  decrease with the substitution of a smaller ion at the Ln<sup>3+</sup> site. The value of  $Q \times f$  increases with the decrease in ionic radius of the lanthanide. Similar variations in dielectric properties were observed by Fukuda *et al.*<sup>30</sup> However, Nishigaki *et al.*<sup>24</sup> and Sun *et al.*<sup>25</sup> observed an increase in the  $\epsilon_r$  and  $\tau_f$  and a decrease in  $Q$  when the smaller Sr ion was substituted for Ba in BaSm<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub>. The Sr substitution for Ba was reported to suppress the formation

**Table 1** Microwave dielectric properties of BaLn<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub> ceramics

Material	$\epsilon_r$	$Q \times f$ , GHz	$\tau_f$ , ppm K <sup>-1</sup>	Bulk density, g cm <sup>-3</sup>
BaLa <sub>2</sub> Ti <sub>5</sub> O <sub>14</sub>	88.02	2200	+70	4.95
BaPr <sub>2</sub> Ti <sub>5</sub> O <sub>14</sub>	76.48	6700	+37	5.12
BaNd <sub>2</sub> Ti <sub>5</sub> O <sub>14</sub>	77.55	17600	+40	5.14
BaSm <sub>2</sub> Ti <sub>5</sub> O <sub>14</sub>	72.15	24000	-14	5.36

of Ba<sub>2</sub>Ti<sub>9</sub>O<sub>20</sub> and enhance the formation of TiO<sub>2</sub> phase. They reported that the increase in  $\epsilon_r$  and  $\tau_f$  are due to the presence of TiO<sub>2</sub>.

The microstructures of these ceramics, thermally etched at 1200°C for 1 h, show a typical grain size of 2–3 μm (Fig. 2), with BaLn<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub> being the major phase. The presence of secondary phases such as Ba<sub>2</sub>Ti<sub>9</sub>O<sub>20</sub>, TiO<sub>2</sub>, etc. is very common<sup>16–20</sup> in these types of compounds. The bulk densities of the samples are given in Table 1 but the presence of the secondary phases precludes the comparison of experimental density with theoretical density. The presence of secondary phases alters the  $\epsilon_r$ ,  $\tau_f$ , and  $Q_u$  values and, in certain cases, improves the dielectric properties. For example, the presence of a small amount of TiO<sub>2</sub> ( $\epsilon_r = 100$ ;  $Q = 10\,000$ ;  $\tau_f = +420$  ppm K<sup>-1</sup>) increases the  $\epsilon_r$  and  $Q$  values and brings the  $\tau_f$  towards positive in negative  $\tau_f$  materials.

## CONCLUSIONS

BaLn<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub> (Ln = La, Pr, Nd, Sm) ceramics have been prepared by the conventional solid state ceramic route. The BaSm<sub>2</sub>Ti<sub>5</sub>O<sub>14</sub> composition with  $\epsilon_r$  of 72.15,  $Q \times f$  of 24 000, and  $\tau_f$  of -14 ppm K<sup>-1</sup> is a useful material for application in cellular telephones.

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