

# A COMPACT VERY-HIGH-PERMITTIVITY DIELECTRIC-EYE RESONATOR ANTENNA FOR MULTIBAND WIRELESS APPLICATIONS

Elinu Paul,<sup>1</sup> S. Mridula,<sup>1</sup> P. Mohanan,<sup>1</sup> P. V. Bijumon,<sup>2</sup> and M. T. Sebastian<sup>2</sup>

<sup>1</sup> Centre for Research in Electromagnetics and Antennas (CREMA)

Department of Electronics

Cochin University of Science and Technology

Kochi 682 022, Kerala, India

<sup>2</sup> Ceramics Technology Division

Regional Research Laboratory

Thiruvananthapuram 695 019, Kerala, India

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**ABSTRACT:** *A very-high-permittivity ( $\epsilon_r = 100$ ) multiband dielectric-eye resonator antenna is presented. The compact antenna, excited by a microstrip line, resonates at two frequencies centered around the 1.9-GHz and 2.4-GHz bands with identical polarization. The behavior of the antenna at different positions along the feed line is studied and optimized. Multiple resonances with the same polarization and broad radiation patterns suggest the suitability of the antenna for multiband wireless applications. © 2004 Wiley Periodicals, Inc. Microwave Opt Technol Lett 43: 118–121, 2004; Published online in Wiley InterScience (www.interscience.wiley.com). DOI 10.1002/mop.20394*

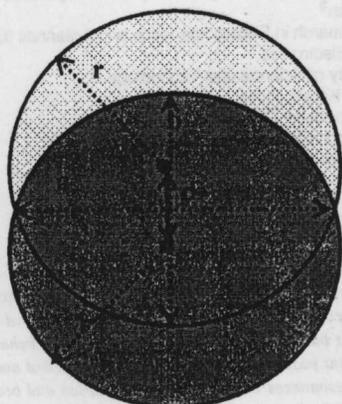
**Key words:** dielectric resonator antenna; multiband wireless applications

### 1. INTRODUCTION

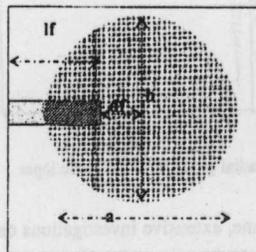
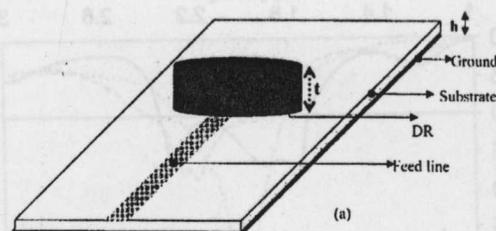
The development of numerous mobile-communication systems has led to increased demand for compact, efficient antennas. Small integrated antennas play a significant role in the progress of the rapidly expanding military and commercial communications applications. Recently, with the booming wireless mobile-communications market, the urgency to design compact multiband antennas is even more pronounced [1–3]. Dielectric resonator antennas (DRAs) are attractive to antenna designers due to their excellent radiation characteristics. In addition, this class of antennas exhibits all the desirable characteristics of a microstrip antenna. Since its inception in the early 1980s, there has been a steady progress of research in this area over the years [4–6]. S. Mridula et al. [7] studied the reflection and radiation characteristics of a microstrip-line-excited rectangular DRA. In this paper, we propose an eye-shaped DRA suitable for wireless applications.

### 2. ANTENNA GEOMETRY

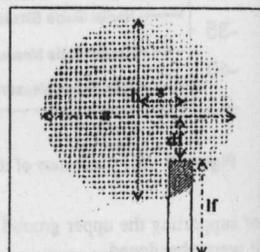
The antenna is comprised of an eye-shaped dielectric resonator (DR), excited directly by a 50Ω microstrip line of width 3 mm and fabricated on a substrate of dielectric constant  $\epsilon_r = 4.28$  and thickness 1.6 mm. The DR is made of very high permittivity ( $\epsilon_r = 100$ ) ceramic material  $\text{TiO}_2$  doped with 1 mole %  $\text{Fe}_2\text{O}_3$  prepared using conventional solid-state ceramics. The eye shape is defined by the intersection of two identical circles of radius 31.5 mm with their centers displaced by 7.5 mm, as shown in Figure 1. A broadband dual-frequency oval-shaped microstrip antenna was proposed by M. Deepukumar et al. [8]. This novel geometry provides two independent ports with orthogonal polarization and excellent isolation between the two ports. However, in this paper dual-band operation is obtained by exciting the various resonant modes of the eye-shaped DRA by using a single feed. The DR can be placed in two orthogonal orientations upon the feed line. Figure 2 illustrates the two configurations of the antenna. To the best knowledge of the authors, a DRA with this novel geometry has not been reported until now.



**Figure 1** Two identical circles of radius  $r$  and center-to-center spacing  $d$ , intersecting to form the eye geometry ( $r = 31.5$  mm,  $d = 7.5$  mm,  $a = 30.5$  mm,  $b = 23.5$  mm)



(b)

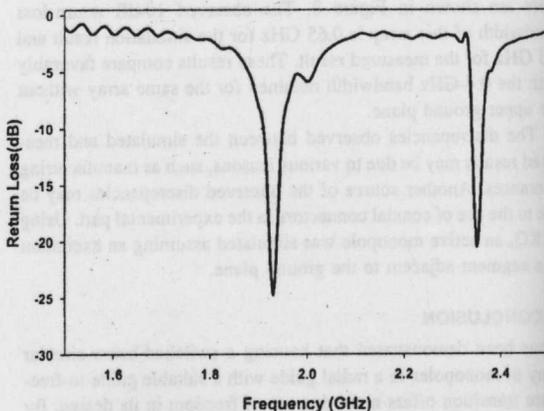


(c)

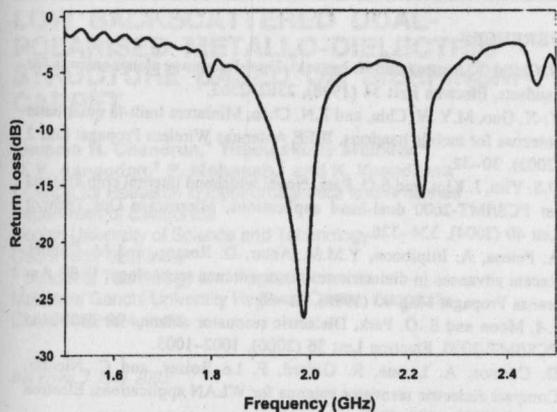
**Figure 2** Geometry and configuration of the DRA: (a) geometry of the proposed eye DRA ( $h = 1.6$  mm,  $t = 7.5$  mm); (b) top view of configuration 1 ( $a = 30.5$  mm,  $b = 23.5$  mm,  $lf = 35$  mm,  $df = 12.5$  mm); (c) top view of configuration 2 ( $a = 30.5$  mm,  $b = 23.5$  mm,  $lf = 35$  mm,  $df = 6$  mm,  $s = 7.5$  mm)

### 3. EXPERIMENTAL RESULTS

The DR is excited directly by a microstrip line of length 35 mm. It is moved symmetrically along the feed line and the variation in return loss as a function of frequency is studied for various positions. The measurements are repeated for the orthogonal orientation of the DR upon the feed line. Numerous resonant modes of the DRA are observed, with the most prominent being the bands centered around  $\sim 1.9$  and  $\sim 2.4$  GHz. The position of the DR along the feed line is experimentally optimized for minimum return loss. The return loss at the optimum position of the DR is plotted in Figure 3 for configuration 1. The antenna exhibits 2.4% and 0.97% 2:1 VSWR bandwidth at these two frequencies, respectively.



**Figure 3** Return loss at the optimum symmetrical position of the DR placed in configuration 1:  $F_1 = 1.93$  GHz (1.907–1.958 GHz) at 2.4% bandwidth;  $F_2 = 2.353$  GHz (2.343–2.365 GHz) at 0.97% bandwidth



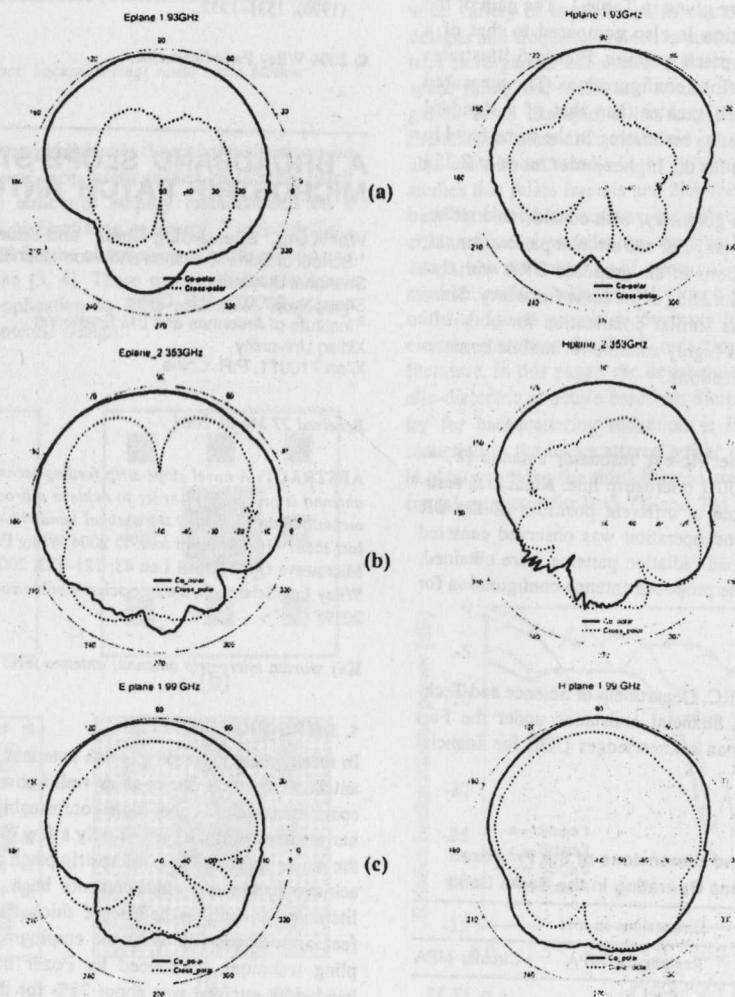
**Figure 4** Return loss at the asymmetrical position of the DR placed in configuration 2:  $F_1 = 1.99$  GHz (1.917–2.02 GHz) at 5.17% bandwidth;  $F_2 = 2.23$  GHz (2.215–2.245 GHz) at 1.1% bandwidth

**TABLE 1** 3-dB Beamwidth of the Proposed Antenna in Different Configurations

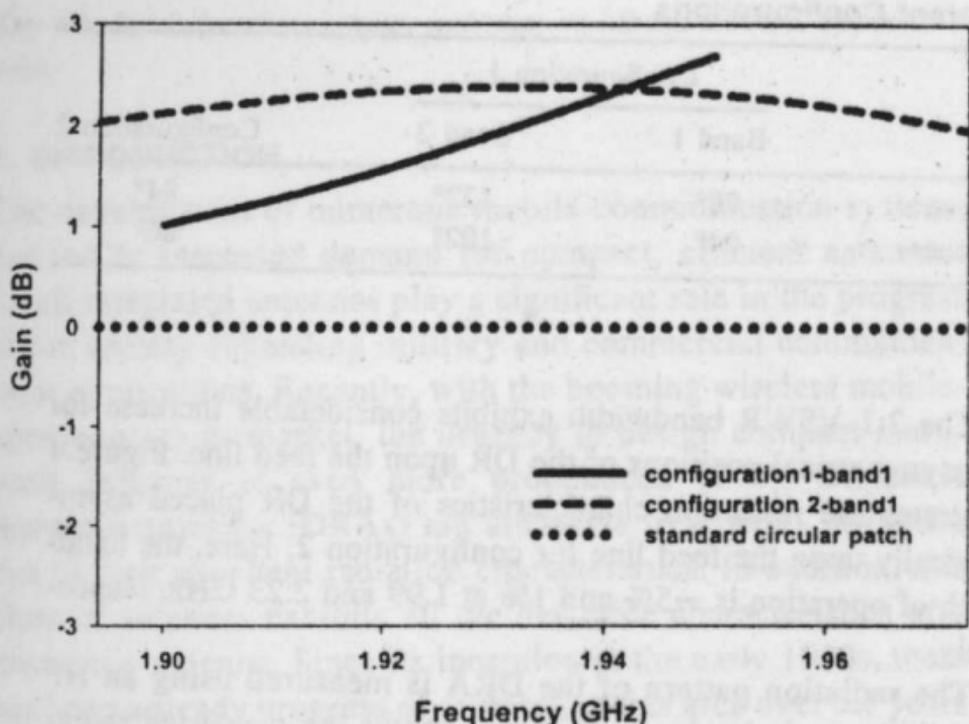
	Configuration 1		Configuration 2
	Band 1	Band 2	
E-plane	98°	122°	84°
H-plane	94°	102°	86°

The 2:1 VSWR bandwidth exhibits considerable increase for the asymmetrical positions of the DR upon the feed line. Figure 4 illustrates the reflection characteristics of the DR placed asymmetrically upon the feed line for configuration 2. Here, the bandwidth of operation is  $\sim 5\%$  and  $1\%$  at 1.99 and 2.23 GHz, respectively.

The radiation pattern of the DRA is measured using an HP 8510C Network Analyser. Figure 5 shows the measured radiation patterns of the DRA. The patterns are reasonably broad in both E- and H-planes, thus indicating the usefulness of the proposed antenna configuration for wireless applications. The



**Figure 5** Radiation patterns of the DRA placed in different configurations: (a) configuration 1 in the first band centered at  $f = 1.93$  GHz; (b) configuration 1 in the second band centered at  $f = 2.353$  GHz; (c) configuration 2 in the band centered at  $f = 1.99$  GHz



**Figure 6** Gain of the proposed antenna placed in different configurations

3-dB beamwidths obtained are given in Table 1. The gain of the proposed antenna configuration is also compared to that of a standard circular microstrip patch antenna. Figure 6 illustrates the gain of the antenna in various configurations. The measured gain of the antenna is  $\sim 2$ -dB greater than that of a standard circular microstrip patch antenna resonating in the same band in all the configurations, except for the higher-order mode at 2.353 GHz.

The antenna is compact in geometry, with considerable reduction in area as compared to rectangular and circular patch antennas. Table 2 compares the dimensions of the proposed DRA with that of other microstrip patches resonating at the same frequency. Since the proposed antenna exhibits similar polarization for both 1.9-GHz and 2.4-GHz bands, it is highly suitable for mobile communications and Bluetooth applications.

#### 4. CONCLUSION

A very-high-permittivity dielectric-eye resonator antenna ( $\epsilon_r = 100$ ) has been excited by a  $50\Omega$  microstrip line. Numerous resonant modes have been excited at different positions of the DR along the feed line. Dual-band operation was observed centered around 1.9 and 2.4 GHz. Broad radiation patterns were obtained, suggesting the relevance of the proposed antenna configuration for wireless applications.

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**TABLE 2** Comparison of the Dimensions of the Proposed Antenna with Patch Antennas Operating in the Same Band

Resonant Frequency	Dimensions in mm		
	Eye DRA	Rectangular MPA	Circular MPA
1.9 GHz	$a = 30.5,$ $b = 23.5,$ $t = 7.5$	$L = 37.8,$ $W = 48.6$	$r = 22.35$
2.4 GHz		$L = 29.8,$ $W = 38.5$	$r = 17.7$

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